Pure rotational CARS thermometry studies of low-temperature oxidation kinetics in air and ethene–air nanosecond pulse discharge plasmas

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Abstract
Pure rotational CARS thermometry is used to study low-temperature plasma assisted fuel oxidation kinetics in a repetitive nanosecond pulse discharge in ethene–air at stoichiometric and fuel lean conditions at 40 Torr pressure. Air and fuel–air mixtures are excited by a burst of high-voltage nanosecond pulses (peak voltage, 20 kV; pulse duration, ∼ 25 ns) at a 40 kHz pulse repetition rate and a burst repetition rate of 10 Hz. The number of pulses in the burst is varied from a few pulses to a few hundred pulses. The results are compared with the previously developed hydrocarbon–air plasma chemistry model, modified to incorporate non-empirical scaling of the nanosecond discharge pulse energy coupled to the plasma with number density, as well as one-dimensional conduction heat transfer. Experimental time-resolved temperature, determined as a function of the number of pulses in the burst, is found to agree well with the model predictions. The results demonstrate that the heating rate in fuel–air plasmas is much faster compared with air plasmas, primarily due to energy release in exothermic reactions of fuel with O atoms generated by the plasma. It is found that the initial heating rate in fuel–air plasmas is controlled by the rate of radical (primarily O atoms) generation and is nearly independent of the equivalence ratio. At long burst durations, the heating rate in lean fuel air–mixtures is significantly reduced when all fuel is oxidized.

1. Introduction
The last decade has seen greatly increased activity in the general discipline that has come to be known as plasma assisted combustion (PAC). Driven by a need to develop more efficient ignition and flame holding systems that can operate over a wide range of pressures, flow velocities and equivalence ratios, numerous groups have reported the use of a variety of non-equilibrium discharge-based ignition techniques and devices, a thorough recent review of which has been recently presented by Starikovskaia [1]. One particular approach, which offers several advantages over conventional dc, rf and microwave discharges, is to utilize high peak voltage nanosecond pulse duration discharges, operated at high pulse repetition rates, on the order of 10–100 kHz. Such discharges are characterized by inherently high reduced electric fields, $E/n$, up to several hundred Townsend (Td). At these high reduced field strengths a significant fraction of the total discharge energy goes into molecular dissociation and population of excited electronic states. Repetitively pulsed nanosecond discharges exhibit increased stability at significantly higher pressures compared with other types of electric discharges, due to the inherent very low duty cycle operation. The basic idea is to operate the discharge with individual pulse duration that is much shorter than characteristic time scales for the onset of ionization instabilities, and with a pulse repetition rate that is greater than the rate of plasma decay. Such an approach enables the generation of large volume, diffuse discharges at relatively high pressures, on the order of 100 Torr (13 900 Pa) in nitrogen, air and oxygen–helium mixtures [2, 3].
Several groups have recently reported the use of nanosecond pulse discharges for fundamental studies of plasma enhanced combustion [4]. For example, Bozhenkov et al [5] have shown significant ignition delay time reduction (by more than one order of magnitude) using a single-pulse nanosecond discharge in H2/air mixtures diluted in argon and preheated to ~900 K in a shock tube. Kim et al [6] have reported large increases in the critical co-flow velocity, leading to lift-off of a methane–air jet diffusion flame. Kim et al [7] have also found increased NO production in premixed methane–air PAC flames, most likely due to excited metastable species reactions, such as O + N2 → NO + N. Similar flame stability limit extension has been reported by Pilla et al [8], who demonstrated significant reduction in the lean flammability limit in a premixed propane–air flame, down to ϕ = 0.3.

Repetitively pulsed nanosecond discharge plasmas also serve as an ideal method for the study of low rotational–translational temperature, non-equilibrium air chemistry and fuel oxidation kinetics. Similar to traditional flash photolysis sources, nanosecond pulsed discharges in air/fuel mixtures generate initial pools of important radical and metastable state excited species, such as N2(A 3Σ), O2(a 1Δ), O, H and R (where R represents any hydrocarbon radical), on time scales of ∼0.1–1.0 μs. Since the energy directly deposited into translational–rotational modes in such discharges is fairly low, single-pulse or repetitive nanosecond pulsing provides a test bed for the study of low-temperature plasma chemical kinetic processes in air and hydrocarbon–air mixtures. For example, Uddi et al [9] have used two photon absorption laser induced fluorescence (TALIF) to obtain time- and space-resolved measurements of absolute atomic oxygen concentration after initiation of single-pulse, ∼20 kV peak voltage, ∼25 ns pulse duration discharge in air, methane–air and ethene–air mixtures at 60 Torr (7895 Pa). The results were found to agree well with predictions of a hydrocarbon–air plasma chemistry model, supplemented by GRI Mech 3.0 [10] and the hydrocarbon oxidation mechanism developed by Wang et al [11]. In particular, Uddi et al concluded that O atoms were primarily created by dissociating collisions of ground electronic state O2 with metastable excited electronic states of N2, a result which is consistent with that recently reported by Stancu et al [12, 13] who studied an atmospheric pressure, nanosecond pulse discharge in a pin-to-pin electrode configuration. Finally, in a separate study, Uddi et al used single photon laser induced fluorescence (LIF) to determine NO concentration as a function of time after a single 25 ns discharge pulse [14]. It was found that the rise in NO concentration occurred on time scales that were approximately two orders of magnitude too fast to be explained by the well-known equilibrium Zeldovich reaction mechanism, but two orders of magnitude too slow to be described by well-known non-equilibrium air chemistry processes, such as reaction of O2 with electronically excited nitrogen atoms, N(2P, 2D). The authors concluded that processes involving reactions of atomic oxygen with vibrationally excited ground electronic state N2, such as that discussed by Gordiets et al [15], and Guerra and Loureiro [16], provide a possible explanation of these recent experimental results.

Single-pulse O atom and N2(A 3Σ) concentration measurements summarized above have served to validate modelling predictions for some of the most important low-temperature plasma oxidation processes. However, since the energy coupled to the plasma by a single nanosecond pulse is fairly low (of the order of ∼1 mJ pulse−1 or ∼0.1 mJ cm−3 pulse−1), detectable heat release requires from a few tens to a few hundred pulses generated at high pulse repetition rate (∼10–100 pulses ms−1). The kinetic mechanism for net energy release in low-temperature hydrocarbon–air plasmas, in excess of that produced directly by the discharge, has not been previously studied in any detail.

In this paper we present time-resolved measurements of rotational–translational temperature rise in air and ethene–air mixtures at 40 Torr (5260 Pa) pressure, excited by a burst of 10 to approximately 600 high voltage, nanosecond duration pulses, at 40 kHz pulse repetition rate. Temperature rise as a function of the number of pulses within the burst is determined by pure rotational coherent anti-Stokes Raman scattering (CARS). Experimental results, both in air and in stoichiometric and lean air–fuel mixtures, are found to agree well with plasma chemistry kinetic modelling calculations. The kinetic model incorporates a new model for energy coupling in nanosecond pulse plasmas [17], low-temperature hydrocarbon–air plasma chemistry model and quasi-one-dimensional heat transfer. In particular, it is found that fairly rapid reactions of ethene with atomic oxygen at room temperature, such as C2H4 + O → CH3 + HCO (k = 4.9 × 10−13 cm3 s−1) and C2H5 + O → CH3CHO + H (k = 2.6 × 10−13 cm3 s−1) [10], initiate additional net exothermic plasma chemical fuel oxidation processes, resulting in additional heat release and, under some conditions, ignition.

2. Experimental

The experiments presented here have been conducted in a rectangular cross section quartz channel/plasma flow reactor 220 mm long × 22 mm width × 10 mm height, with 1.75 mm thick walls (see figure 1). The measurements have been conducted in dry air and in mixtures of dry air with ethene. Flow rates of air and fuel are controlled by mass flow controllers at a pressure of 40 Torr and a flow velocity of approximately u = 0.8 m s−1. Two rectangular copper plate
Figure 2. Typical single-pulse voltage waveforms during a burst of nanosecond pulses in air at 40 Torr and pulse repetition rate 40 kHz (pulse #100 in a burst), for grounded and floating discharge operation.

For all measurements presented in this paper, the discharge was operated at 40 kHz pulse repetition rate. In most of the measurements, the pulse generator was operated in repetitive burst mode, generating sequences of up to 1000 pulses at a pulse repetition rate of 40 kHz and a burst repetition rate of 40 kHz, for grounded and floating discharge operation. It can be seen that leaving the positive terminal floating somewhat reduces the pulse duration (from ∼25 ns to ∼10 ns for the negative voltage pulse) and considerably reduces voltage oscillations after the pulse, only weakly affecting the peak voltage (22–23 kV). It was also found that leaving the positive terminal floating considerably improved the discharge stability.

electrodes are attached to the outside of the quartz channel, as shown in figure 1. The electrode plates are 14 mm wide by 65 mm long, and are rounded at the corners to reduce the electric field non-uniformity. Room temperature flow residence time in the discharge region is approximately 75 ms, based on the flow velocity of 0.8 m s⁻¹. High voltage, nanosecond pulse discharge (20 kV peak voltage, ∼25 ns pulse duration) is generated in air and premixed ethene–air flows using a Chemical Physics Technologies high-voltage pulsed power supply. The power supply generates negative polarity pulses, while the terminal connected to the positive electrode can be grounded or left floating. Figure 2 shows typical single-pulse voltage waveforms during a burst of nanosecond pulses in air at 40 Torr and pulse repetition rate 40 kHz (both for pulse #100 in a burst), for grounded and floating discharge operation. It can be seen that leaving the positive terminal floating somewhat reduces the pulse duration (from ∼35 ns to ∼25 ns for the negative voltage pulse) and considerably reduces voltage oscillations after the pulse, only weakly affecting the peak voltage (22–23 kV). It was also found that leaving the positive terminal floating considerably improved the discharge stability.

For all measurements presented in this paper, the discharge was operated at 40 kHz pulse repetition rate. In most of the measurements, the pulse generator was operated in repetitive burst mode, generating sequences of up to 1000 pulses at a pulse repetition rate of 40 kHz and a burst repetition rate of 10 Hz. This rate matches the pulse repetition rate of the diagnostic lasers, and ensures that each gas sample in the flowing discharge cell experiences only a single burst. To produce breakdown in the discharge section on the first pulse, the test cell was irradiated by a deuterium UV lamp (Resonance Ltd) through the side wall, providing pre-ionization of the discharge volume. The equivalence ratio in air–fuel mixtures was varied from φ = 0.1 to 1.0.

A schematic of the pure rotational CARS apparatus, patterned after that of Alden et al [18], is shown in figure 3. Briefly, an Nd : YAG pumped broadband Ti : sapphire laser, patterned after that of Finkelstein et al [19] but modified for broad spectral output, with a centre wavelength of approximately 780 nm and pulse duration of approximately 15 ns is split into two ‘pump’ beams, with approximately 20 mJ each, and orthogonal linear polarizations. The spectral intensity characteristics of the Ti : sapphire output are illustrated in figures 4(a)–(c). Figure 4(a) shows the spectrum from a typical single Ti : sapphire pulse, whereas figures 4(b) and (c) show 10 and 100 pulse averages, respectively. Note that the longitudinal mode spacing of the Ti : sapphire cavity is ∼150 MHz (0.005 cm⁻¹) corresponding to ∼40 000 modes contained within the full width half maximum (FWHM) of the spectral profile. While the spectral intensity profile can be seen to be relatively smooth, it is known that phase fluctuations, which cannot be discerned in figure 4, contribute significantly to the statistical noise in dual broadband pure rotational CARS spectra [20].

The second harmonic output (532 nm) of a second Nd : YAG laser, with 10 ns pulse duration, is used to generate a horizontally polarized ‘probe’ beam. The pump and probe beams are overlapped in a focused linear phase matching geometry, using a 400 mm focal distance lens. The overlapped focused beams, which propagate parallel to the major axis of the electrodes, form an approximately cylindrically shaped measurement region ∼0.1 mm in diameter and 1–2 mm long in the plasma. The pure rotational CARS signal beam is generated with vertical polarization, which allows for very significant (more than a factor of 1000) discrimination from stray, horizontally polarized, probe light using a right angle polarizer. There is, however, a reduction in CARS resonant and non-resonant intensities by a factor of 9/16 and 1/9, respectively. This is most easily seen from equations (2), (5), (6) and (7) of Vestin et al [21]. Skipping the details, the use of this polarization scheme results in zero contribution to the CARS field (both resonant and non-resonant) from susceptibility elements χ_1122 and χ_1111. The magnitude of the remaining χ_1212 contribution is a factor of 3/2 (resonant) and 1/2 (non-resonant) of that when all fields are aligned parallel to one another. This reduced CARS field (both resonant and non-resonant contributions) is aligned parallel to the detection polarizer (i.e. orthogonal to the probe field), as can be seen from inspection of equation (7) of [21] with θ = 90° and φ = 0°. The CARS beam, after transmission through a short wavelength pass coloured glass filter to eliminate residual pump scattering, is focused onto the entrance slit of a 1/2 meter spectrometer, with an 1800 lines mm⁻¹ grating and a gated ICCD camera (Princeton Instruments–PI-MAX). The spectrometer wavelength axis is calibrated using a standard Hg vapour pen lamp. The spectral resolution of the CARS signal is ∼1–2 Å. Typically, the CARS signal was averaged over 300 bursts (30 s).

Inference of rotational temperature is performed using the Sandia National Laboratories CARS code [22]. Prior
Figure 3. Schematic diagram of pure rotational CARS apparatus. Electrodes are above/below plane of paper.

Figure 4. Broadband Ti:sapphire spectral output and intensity correction factor for experimental CARS spectra.

Experimental CARS spectra are divided by this correction factor prior to temperature inference. Note that the Sandia CARS code actually fits the square root of the experimental spectrum, corresponding to the third order susceptibility, also known as $\chi_{\text{CARS}}$. Note also that the CARS spectra were fitted, experimental spectra are corrected to account for the finite spectral width of the Ti:sapphire pump laser. Figure 4(d) shows the product $I(v) \cdot I(v + \Delta v)$, averaged over the broadband laser spectrum shown in figure 4(c) and normalized to $I^2(\Delta v = 0) = 1$, as a function of $\Delta v$. 
modelled as pure air as it was experimentally determined that the contribution of ethene to the pure rotational CARS signal was negligible, even at $\phi = 1$.

In addition to CARS measurements, spatially averaged rotational temperature in the plasma is inferred from visible emission spectra (partially rotationally resolved $0 \rightarrow 0$ band of the $N_2(C^3\Pi_u \rightarrow B^3\Pi_g)$ band system) as a function of time during the pulse burst. The emission spectroscopy measurement utilizes a $\frac{1}{2}$ meter spectrometer, with a 2400 lines mm$^{-1}$ grating, and a gated ICCD camera. Emission spectra were obtained in the range 0–20 ms with respect to initiation of a single discharge burst, and averaged over 0.5–1.0 ms (20–40 pulses). The uncertainty of these temperature measurements ranges from ±30 °C in air to ±50 °C in ethene–air (at $T = 0$–500 °C) and to ±100–150 °C in ethene–air (at $T \sim 1000$ °C). The uncertainty in CARS inferred rotational temperatures will be discussed in section 4.

Finally, in order to gauge the uniformity of the nanosecond pulsed discharge, the gated ICCD camera was also used to obtain qualitative UV visualization images of a single discharge pulse as a function of pulse number within a burst.

### 3. Hydrocarbon–air nanosecond pulsed discharge and plasma chemistry model

The hydrocarbon–air nanosecond pulsed discharge model used in this work is similar to that described by Uddi et al [9, 14]. The air plasma chemistry model incorporates a set of equations for number densities of neutral species ($N$, $N_2$, $O$, $O_2$, $O_3$, NO, NO$_2$, $N_2$O, NO$_2$), charged species ($e^-$, $N^+$, $N_2^+$, $N_2^+_1$, $N_2^+_2$, $O^-$, $O_2^-$, $O_3^-$, NO$^-$, NO$_2^-$, $N_2$O$^-$, $N_2$O$_2^-$, $N_2$NO$^-$, $N_2$NO$_2^-$, NONO$^-$, $O^+$, $O_2^+$, $O_3^+$, NO$^+$, NO$_2^+$, $N_2$O$^+$) and excited species ($N_2(A^3\Sigma)$, $N_2(B^3\Pi)$, $N_2(C^3\Pi)$, $N_2(a^1\Sigma)$, $O_2(a^1\Delta)$, $O_2(b^3\Sigma)$, $O_2(e^3\Sigma)$, $N^2(\text{D})$, $N^2(\text{P})$, $O(1\text{D})$ produced in the plasma [23]. The dominant neutral species in air plasmas are the excited electronic states of nitrogen, which are formed by electron impact excitation, and O atoms, which are formed by electron impact dissociation of oxygen and by collisional quenching of excited nitrogen by oxygen, as well as ozone. The species concentration equations are coupled with the two-term expansion Boltzmann equation [24] for the energy distribution function of plasma electrons. The Boltzmann equation solver uses electron impact cross sections [25, 26] and calculates the electron energy distribution function, as well as the rate coefficients of electron impact ionization, dissociation and electronic excitation, used by the rest of the model. Rate coefficients of remaining kinetic processes in the air plasma, such as electron recombination, attachment and detachment, ion–molecule reactions and reactions of excited electronic species are taken from [23]. The list of air plasma processes incorporated into the model and their rates is summarized in [14].

To model hydrocarbon–air plasma processes, the air plasma kinetic model was supplemented with methane and ethene dissociation by electron impact and in reactions with electronically excited nitrogen molecules. Cross sections and rate coefficients of these reactions, listed in table 1, were taken from [27–35]. Finally, the plasma model was combined with the hydrocarbon oxidation mechanism, GRI Mech 3.0 [10].

The high-voltage pulse shape used by the plasma chemistry model is a Gaussian fit to the negative polarity voltage pulse shown in figure 2. However, due to strong shielding of the applied voltage charge accumulation on the quartz channel walls, the field in the plasma after breakdown is much lower than the applied field. In our previously reported work [9, 14], this effect was incorporated by allowing the peak reduced electric field in the pulsed plasma to be an adjustable parameter, chosen to reproduce the experimentally determined peak O atom number density measured in air at $P = 60$ Torr and $T = 300$ K. From the previous work, the best fit value for peak effective reduced electric field was found to be $(E/N)$_{peak} = 250 Td (1 Td = $10^{-17}$ V cm$^2$), with the corresponding coupled pulse energy of 0.76 mJ. Figure 5, taken from [9], compares time-dependent TALIF O atom concentration measurements in single-pulse nanosecond discharges in air and ethene–air at $\phi = 0.5$. It can be seen that in both cases, the experimental data are in excellent agreement with the model prediction. It is stressed that no additional adjustable parameters were used to obtain the level of agreement shown for the ethene–air data set, other than the 0.76 mJ coupled pulse energy as determined from the air discharge data. In addition, while not shown, similarly excellent agreement was found for O atom concentration versus time in a stoichiometric methane–air mixture, again excited by a single nanosecond discharge pulse [9].

While the previous results have provided a validation for the critical elements of the air chemistry portions of the model, the hydrocarbon oxidation portion is clearly only partially validated, as O atom production and loss is just one, albeit important, process in the chain of processes that lead to

<table>
<thead>
<tr>
<th>Process</th>
<th>Rate</th>
<th>Reference</th>
</tr>
</thead>
<tbody>
<tr>
<td>$\text{CH}_4 + e^- \rightarrow \text{CH}_3 + H + e^-$</td>
<td>$\sigma$</td>
<td>[27]</td>
</tr>
<tr>
<td>$N_2(A^3\Sigma) + \text{CH}_4 \rightarrow N_2 + \text{CH}_3 + H$</td>
<td>$3.3 \times 10^{-15}$ cm$^3$ s$^{-1}$</td>
<td>[29]</td>
</tr>
<tr>
<td>$N_2(B^3\Pi) + \text{CH}_4 \rightarrow N_2 + \text{CH}_3 + H$</td>
<td>$3.0 \times 10^{-10}$ cm$^3$ s$^{-1}$</td>
<td>[30]</td>
</tr>
<tr>
<td>$N_2(C^3\Pi) + \text{CH}_4 \rightarrow N_2 + \text{CH}_3 + H$</td>
<td>$5.0 \times 10^{-10}$ cm$^3$ s$^{-1}$</td>
<td>[31]</td>
</tr>
<tr>
<td>$N_2(a^1\Sigma) + \text{CH}_4 \rightarrow N_2 + \text{CH}_3 + H$</td>
<td>$3.0 \times 10^{-10}$ cm$^3$ s$^{-1}$</td>
<td>[32]</td>
</tr>
<tr>
<td>$C_2H_4 + e^- \rightarrow \text{products} + e^-$</td>
<td>$\sigma$</td>
<td>[28]</td>
</tr>
<tr>
<td>$N_2(A^3\Sigma) + C_2H_4 \rightarrow N_2 + C_2H_3 + H$</td>
<td>$9.7 \times 10^{-11}$ cm$^3$ s$^{-1}$</td>
<td>[33]</td>
</tr>
<tr>
<td>$N_2(B^3\Pi) + C_2H_4 \rightarrow N_2 + C_2H_3 + H$</td>
<td>$3.0 \times 10^{-10}$ cm$^3$ s$^{-1}$</td>
<td>estimate</td>
</tr>
<tr>
<td>$N_2(C^3\Pi) + C_2H_4 \rightarrow N_2 + C_2H_3 + H$</td>
<td>$3.0 \times 10^{-10}$ cm$^3$ s$^{-1}$</td>
<td>estimate</td>
</tr>
<tr>
<td>$N_2(a^1\Sigma) + C_2H_4 \rightarrow N_2 + C_2H_3 + H$</td>
<td>$4.0 \times 10^{-10}$ cm$^3$ s$^{-1}$</td>
<td>[35]</td>
</tr>
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</table>

*Table 1. Fuel species dissociation processes.*
fuel oxidation and heat release. Since temperature rise in a single discharge pulse under our conditions is estimated to be small, on the order of \( \sim 1–2 \text{ K} \), the temperature measurements presented in this paper are performed with the discharge operating in ‘burst’ mode at a high pulse repetition rate.

Kinetic modelling of the burst mode discharge plasma required two key changes in the model. First, as demonstrated in greater detail in a recent paper by Adamovich et al. [17], specific energy coupled to the plasma by a nanosecond discharge pulse (in eV molecule\(^{-1}\)) remains approximately constant, i.e. coupled pulse energy varies approximately linearly with number density. Briefly, the nanosecond pulse discharge energy coupling model developed in [17] incorporates key effects of pulsed breakdown, charge accumulation on dielectric surfaces and sheath development on nanosecond time scale. Basically, the model predicts that energy coupled to the plasma during an individual nanosecond pulse burst results in breakdown voltage reduction, thereby decreasing the pulse energy coupled to the plasma as a function of the pulse number within the burst. For the discharge geometry and pulse voltage waveform used in this work, the coupled pulse energy scales, and would require massive computational resources.

The second model modification accounts for energy loss due to conduction to the quartz channel walls. This is described by incorporating a conduction heat transfer term into the energy equation [17]:

\[
\frac{dT}{dt} = \frac{q(T) - (T - T_w)}{\rho c_p (L/\pi)^2} = q_{\text{rep}} - \frac{1}{\rho c_p} \sum_{i} h_i \left( \frac{dn_i}{dt} \right) - \frac{\lambda(T) (T - T_w)}{\rho c_p (L/\pi)^2},
\]

where \( q = Q_{\text{coupled}} A L / \rho c_p \) is the coupled pulse energy per unit mass, \( q_{\text{rep}} \) is the pulse repetition rate in a burst, \( h_i \) are enthalpies of chemical and excited species, \( dn_i / dt \) are the rates of species concentrations (in kmole m\(^{-3}\)) change in chemical reactions, \( \lambda(T) \) is the thermal conductivity, \( T_w = 300 \text{ K} \) is the wall temperature, \( L \) is the channel height and \( L/\pi \) is the spatial scale for conduction heat transfer with uniform generation in the rectangular geometry. Applicability of a 0D approximation for time-dependent conduction heat transfer was validated by solving separately a 1D unsteady heat transfer equation [17],

\[
\frac{dT}{dt} = \frac{1}{\rho c_p} \frac{\partial}{\partial x} \left( \lambda(T) \frac{dT}{dx} \right)
\]

with the same initial and boundary conditions, and the rate of temperature rise \( \dot{q} = q_{\text{rep}} - \frac{1}{\rho c_p} \sum_{i} h_i \left( \frac{dn_i}{dt} \right) \) being the same as predicted by the plasma chemistry model. Comparing the time-dependent plasma temperature, \( T(t) \), obtained by the plasma chemistry model using equation (2) with the spatially averaged temperature obtained by solving equation (3), \( T(t) = \frac{1}{L} \int_{0}^{L} T(x, t) \, dx \), shows that the difference between them does not exceed a few per cent.

4. Results and discussion

Discharge uniformity measurements. Figure 6 shows a collage of broadband ICCD camera images (primarily \( \text{N}_2 \) second positive band UV/visible emission) of single discharge pulses in pure air at 40 Torr, obtained for different pulse numbers in a burst, ranging from 5 to 600, at a pulse repetition rate of 40 kHz and a burst repetition rate of 10 Hz. In these images, the camera gate was 20 \( \mu \text{s} \). Note that individual images were taken during different bursts and do not illustrate discharge development during a single burst. While some structure is observed for the first few pulses (e.g. see image of pulse #5), all images for pulse numbers exceeding \( \sim 3–5 \) are observed to be extremely uniform, including images obtained for pulse numbers up to 1000 (25 ms burst duration), which are not shown in figure 6. Similar results were obtained for a shorter camera gate, 1 \( \mu \text{s} \). Figure 7 is similar to figure 6, except the images are obtained in a fuel lean (\( \phi = 0.1 \)) ethene–air mixture. In this case the development of a few large scale structures (filaments) in the discharge at pulse numbers \( \sim 50–100 \) is quite apparent. While not shown, comparison of several sets of images obtained from different bursts, but at the same pulse number within the burst, indicates that the filaments develop at random locations within the discharge.

Figure 5. O atom mole fraction versus time after a single high-voltage pulse in air, in methane–air (\( \phi = 1.0 \)) and in ethene–air (\( \phi = 0.5 \)) mixtures at \( P = 60 \text{ Torr} \) [9]. Pulse energy used in modelling calculations, 0.76 mJ.
Figure 6. Collage of broadband ICCD camera images (primarily N$_2$ second positive system emission) of individual discharge pulses in air at 40 Torr, obtained during burst mode operation. Discharge pulse repetition rate is 40 kHz, burst repetition rate 10 Hz, camera gate 20 $\mu$s.

Figure 7. Collage of broadband ICCD camera images of individual discharge pulses in fuel lean ($\phi = 0.1$) ethene–air mixture at 40 Torr, obtained during burst mode operation. Discharge pulse repetition rate is 40 kHz, burst repetition rate 10 Hz, camera gate 20 $\mu$s.

Figure 8. Collage of broadband ICCD camera images of individual discharge pulses in stoichiometric ($\phi = 1.0$) ethene–air mixture at 40 Torr, obtained during burst mode operation. Discharge pulse repetition rate is 40 kHz, burst repetition rate 10 Hz, camera gate 20 $\mu$s.

Our previous nanosecond pulse plasma images [17] suggested that filamentation of fuel–air plasmas most likely occurs due to ionization instability development. These results demonstrated that adding either small amounts of ethene (0.07–0.7%, equivalence ratio $\phi = 0.01$–0.1) or comparable amounts of NO (0.7%) to uniform and stable air plasma readily produced filamentation. Note that both ethene and NO have fairly low ionization potentials, 10.5 eV and 9.3 eV, respectively (compared with nitrogen, 15.6 eV and oxygen, 12.2 eV). In addition, kinetic modelling of a single pulse nanosecond discharge shows that adding either ethene or NO to air results in more rapid heating by the discharge. It is well known that both lowering the ionization potential and increasing the heating rate contribute to accelerating the rate of ionization/heating instability development [36]. Therefore, both of these factors are likely to play key roles in constriction and filamentation of ethene–air plasmas under these conditions. As can also be seen in figure 7, the filaments tend to dissipate after $\sim$ 400 pulses (10 ms), most likely due to higher thermal diffusivity, $\lambda/\rho c_p$, at higher temperatures. Diluting the fuel–air mixture with helium, which has much higher thermal diffusivity, resulted in accelerated dissipation of filaments, again suggesting that they are formed due to ionization/heating instability. For $\phi = 1.0$ the results are similar, as illustrated in figure 8. Again, large scale structures begin to appear after $\sim$50–100 pulses and dissipate after $\sim$ 400 pulses.

Emission spectroscopy results. Figure 9 shows experimentally measured time-resolved spatially averaged rotational temperature, inferred from N$_2$ second positive system emission spectra, in pulsed air plasmas at 40, 60 and 100 Torr, along with kinetic model predictions. ICCD camera imaging [37] showed that the air plasma remains stable and uniform in the entire range of pressures. As discussed in section 2, each emission spectrum has been accumulated over a period of 0.5 ms (i.e. 20 discharge pulses). As discussed in section 3, in the modelling calculations coupled pulse energy, $Q_{\text{coupled}}$, is scaled proportional to the number density in the plasma (see equation (1)). From figure 9, it can be seen that after an initial rise over 10–20 ms (400–800 pulses), the plasma temperature appears to reach a quasi-steady-state, due to increasing heat.
plasma chemistry model prediction. The nanosecond pulse energy coupling model and the plasma chemistry model accurately reproduces the time-dependent spatially averaged temperature in air plasmas in a wide range of pressures and temperatures, providing validation of both the plasma chemistry model and the nanosecond pulse energy coupling model (see figure 1).

It can be seen that the temperature rise becomes more rapid at higher pressures, consistent with the prediction of the nanosecond pulse energy coupling model (see figure 1). The results shown in figure 9 demonstrate that the air plasma chemistry model accurately reproduces the time-dependent spatially averaged temperature in air plasmas in a wide range of pressures and temperatures, providing validation of both the nanosecond pulse energy coupling model and the plasma chemistry model.

Figure 10 compares time-resolved spatially averaged temperature in air and in ethene–air (φ = 1.0) at P = 40 Torr with the plasma chemistry model prediction. Transfer losses which balance energy loading by the discharge. It can also be seen that the temperature rise becomes more rapid at higher pressures, consistent with the prediction of the nanosecond pulse energy coupling model (see figure 1). The results shown in figure 9 demonstrate that the air plasma chemistry model accurately reproduces the time-dependent spatially averaged temperature in air plasmas in a wide range of pressures and temperatures, providing validation of both the nanosecond pulse energy coupling model and the plasma chemistry model.

Figure 10 compares time-resolved spatially averaged temperature in air and in ethene–air (φ = 1.0) at P = 40 Torr with the plasma chemistry model prediction. Transfer losses which balance energy loading by the discharge. It can also be seen that the temperature rise becomes more rapid at higher pressures, consistent with the prediction of the nanosecond pulse energy coupling model (see figure 1). The results shown in figure 9 demonstrate that the air plasma chemistry model accurately reproduces the time-dependent spatially averaged temperature in air plasmas in a wide range of pressures and temperatures, providing validation of both the nanosecond pulse energy coupling model and the plasma chemistry model.

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Pure rotational CARS thermometry measurements. The reliance on spatially averaged rotational temperatures inferred from emission spectroscopy for air–fuel plasma chemistry studies can be misleading, especially under conditions where heat transfer clearly affects the temperature and may result in significant temperature gradient across the plasma, as illustrated in figures 9 and 10. On the other hand, CARS thermometry is a well-known diagnostic technique for high spatial and temporal resolution measurement of temperature distributions in flames and plasmas. Figure 11 shows a typical pair of experimental pure rotational CARS spectra in air and in a stoichiometric ethene–air mixture at P = 40 Torr. Both spectra are obtained approximately 40 μs after a 400 pulse burst at 40 kHz (10 ms burst duration). In these, as well as all subsequent measurements, the laser beams were focused in the centre of the discharge (halfway between the top and bottom electrodes and halfway between the upstream and downstream boundaries of the plasma). The spectra shown in figure 11 are averaged over approximately 300 individual laser shots or over 30 s at laser and plasma burst repetition rates of 10 Hz. For burst sequences with a higher number of pulses, multiple (up to three) accumulations of 300 laser shot spectra are added together to further improve signal to noise, partially compensating for the quadratic dependence of the CARS signal with fluid density. The spectra in figure 11 are also normalized to unity at the highest intensity value. The increase in temperature due to net exothermic plasma-induced fuel oxidation chemistry is readily apparent by comparing the relative intensities at high J values (i.e. at large Raman shifts of ~100–250 cm⁻¹). Figure 12 shows the square root of the experimental ethene–air CARS spectrum from figure 11 along with the best fit synthetic spectrum generated by the Sandia CARS code. While there are some statistical fluctuations that can be seen from the imperfect agreement between the experimental spectrum and best least squares fit, the overall rotational envelop is well reproduced, resulting in an inferred best fit rotational temperature of 860 K. Note that the Sandia CARS code does not provide any estimate of uncertainty in the fitting parameters. We therefore provide an estimate of temperature uncertainty by varying the temperature from that which minimizes the square of the residual between fit and data (χ²) to that which increases it by 20%. For air and fuel
Figure 11. Typical rotational CARS spectra in air and ethene–air ($\phi = 1$) after a 400 pulse burst at 40 kHz (burst duration 10 ms). $P = 40$ Torr. Each spectrum is normalized to peak rotational line intensity.

Figure 12. Experimental and synthetic rotational CARS spectra in ethene–air ($\phi = 1$) at the conditions of figure 11. Inferred rotational temperature $T = 860 \pm 50$ K.

Figure 13. Comparison of experimental spatially averaged (emission) and centreline (CARS) temperatures in a repetitively pulsed nanosecond discharge in air at $P = 40$ Torr with the plasma chemistry model prediction.

Figure 14. Comparison of experimental centreline (CARS) temperatures in a repetitively pulsed nanosecond discharge in air and in ethene–air ($\phi = 0.1$ and $\phi = 1.0$) at $P = 40$ Torr with the plasma chemistry model prediction.

At $t = 15$ ms (600 pulses), the difference between CARS and emission temperature is about 100 °C. In the kinetic model, the spatially averaged temperature is given by equation (2) and the centreline temperature is given by equation (3), and there is good agreement between the model and the experiment in each case. Therefore, using a constant wall temperature boundary condition of $T_w = 300$ K in the plasma chemistry/heat transfer model appears to adequately describe the transverse temperature distribution in the air plasma.

Figure 13 shows time-resolved air plasma temperatures inferred from emission spectra and CARS as well as the plasma chemistry model predictions for a pulse burst discharge at $P = 40$ Torr and 40 kHz pulse repetition rate. Both emission (i.e. spatially averaged) and CARS (centreline) rotational temperatures are very close to each other until approximately 7.5 ms (300 pulses). After this time, the emission temperature rise becomes slower and starts to level off, indicating significant heat transfer losses, while the CARS temperature continues to increase up to 17 ms (680 pulses).
in air during the first 5 ms (200 pulses), approximately 350 °C versus 125 °C. Second, the CARS data show that during this stage the rates of heat release in lean and stoichiometric ethene–air mixtures are very close to each other, although the fuel mole fractions differ by a factor of 10. Third, experimental temperatures in air and in the lean ethene–air mixture reach a quasi-steady-state at \( t \sim 15 \) ms (600 pulses), while temperature in the stoichiometric ethene–air mixture continues to rise.

Two of these trends are well reproduced by the kinetic model. In particular, the model predicts a significantly more rapid centreline temperature rise in air–fuel mixtures than in air, consistent with the CARS data. Also, predicted rates of centreline temperature rise in air–fuel mixtures at \( \phi = 0.1 \) and \( \phi = 1.0 \) are very close to each other until \( t = 5 \) ms. However, the model predicts a significantly lower temperature in the stoichiometric air–fuel mixture at \( t > 5 \) ms than is measured experimentally. Specifically, the model predicts that by 5 ms (200 pulses) the temperature reaches a quasi-steady-state, whereas the CARS data indicate that it continues to rise.

To explain these general trends, it is noted that the rate of heat release in the plasma as a function of the number of pulses in the burst depends significantly on mixture composition. Figure 15, which plots atomic oxygen and ethene mole fractions predicted by the model in air, lean (\( \phi = 0.1 \)) and stoichiometric (\( \phi = 1.0 \)) ethene–air mixtures (i.e. at the conditions of figure 14), provides some insight into these trends. In the absence of fuel, O atoms, which are primarily produced by post-discharge collisional quenching of the metastable electronic state of nitrogen, \( N_2(3 \Sigma) \):

\[
N_2(3 \Sigma) + O_2 \rightarrow N_2 + 2O \quad (4)
\]

and by electron impact during the discharge pulse,

\[
O_2 + e^- \rightarrow O + O + e^- \quad (5)
\]

decay relatively slowly in recombination reactions,

\[
O + O_2 + M \rightarrow O_3 + M \quad (6)
\]

Figure 15. Plasma chemistry model predictions for O (solid curves) and ethene (dashed curves) mole fractions for air and ethene–air mixtures.

Note that at low atomic oxygen mole fraction, O atom decay is primarily due to the three-body recombination process (6), whereas as both O atoms and ozone build up, as a result of repetitive pulsing, the rate of the two-body process (7) begins to dominate.

In air, the relatively low rate of recombination results in a considerable build-up of O atoms, to mole fractions of up to \( \sim 1\% \), which is comparable to the 0.7% initial mole fraction of ethene in the lean air–fuel mixture (\( \phi = 0.1 \)). However, in ethene–air mixtures, O atoms rapidly react with ethene due to the parallel processes,

\[
O + C_2H_4 \rightarrow CH_3 + HCO, \quad (8)
\]
\[
O + C_2H_4 \rightarrow H + CH_2CHO, \quad (9)
\]

which are relatively fast at low temperatures, with 300 K rate coefficients of \( k = 4.9 \times 10^{-13} \text{ cm}^3 \text{s}^{-1} \) and \( k = 2.6 \times 10^{-13} \text{ cm}^3 \text{s}^{-1} \), respectively [9]. These low-temperature reactions of atomic oxygen with ethene initiate a number of net exothermic hydrocarbon reactions, resulting in accelerated temperature rise, which the model accurately predicts, as can be seen in figure 14.

Because of these rapid reactions with ethene, O atom number densities in ethene–air mixtures are much lower than in air under otherwise identical conditions. This can be seen by comparison of the solid red (air) and black (ethene–air, \( \phi = 1 \)) curves in figure 15. Further, as long as fuel is in excess, the rate of chemical energy release (and therefore the rate of temperature rise) in air–fuel mixtures is dictated by the rate of O atom generation (by reactions of equations ((4), (5))), which is only slightly affected by the ethene mole fraction in the mixture (0.7–6.5%). For this reason, the predicted initial heating rates in the lean and stoichiometric ethene–air mixtures are very close to each other, which is again consistent with the experimental CARS temperature measurements shown in figure 14.

After nearly all fuel in the lean mixture has been oxidized (after \( \sim 200 \) discharge pulses or \( \sim 5 \) ms), the heating rate is predicted to slow down, and, simultaneously, the O atom number density is predicted to start rising rapidly. This is illustrated in figure 14 (heating rate reduction) and figure 15 (O atom build-up), respectively. However, since the stoichiometric mixture has ten times more fuel, its mole fraction remains approximately constant (dashed black curve in figure 15), as does the corresponding predicted heating rate. For this reason, the stoichiometric mixture continues to generate additional heat as the number of pulses increases beyond \( \sim 200–400 \) (5–10 ms). The most likely reason for the significant difference between experimental and predicted centreline temperatures in the stoichiometric mixture after a large number of pulses (\( \sim 400 \) pulses or \( \sim 10 \) ms) is heating of the test section walls. Under these conditions, the use of the constant wall temperature boundary condition \( T_w = 300 \text{ K} \) is likely no longer justified, since the rate of heat transfer from the plasma to the cold wall is significantly overestimated. Further temperature measurements, using a vertical translation stage.
to move the discharge cell relative to the fixed CARS beams, will study this effect in greater detail.

Finally, figure 16, taken from Uddi et al [38] compares previously measured O atom number densities in air, stoichiometric methane–air and lean (φ = 0.5) ethene–air at P = 60 Torr as a function of the number of pulses in a burst with predictions of the kinetic model used in this work. These measurements were taken using a different plasma generator (FID Technology) than that used in this work, and at a different pulse repetition rate (100 kHz). However, it can be seen that the model is in good agreement with all three experimental data sets, predicting accumulation of O atoms in air of up to 4 × 10^{15} cm^{-3} (0.2% mole fraction) over 1 ms (100 pulses), and much lower O atom concentration in φ = 0.5 ethene–air, after the same number of pulses, by approximately two orders of magnitude. In fact, the data shown in figure 16 confirm that the rate of O atom production in ethene–air is essentially equal to the rate of loss, due to the relatively fast rates of processes of equations (8) and (9). Note also that while not studied in this work, the rate of loss of O atoms via reaction with methane at room temperature has been confirmed to be many orders of magnitude lower than with ethene [9]. This is reflected in the observed build-up of O atoms during the burst, to a value intermediate between that measured in air and in an ethene–air mixture.

5. Summary and conclusions

Time-resolved rotational temperature in a repetitively pulsed nanosecond discharge operated in burst mode in air and in ethene–air mixtures has been measured by purely rotational CARS. The results are compared with the low-temperature hydrocarbon–air plasma chemistry model predictions. The plasma chemistry model, developed in our previous work, has been validated by a series of atomic oxygen mole fraction measurements taken in low-temperature air, and ethene–air nanosecond pulsed plasmas. In this work, the plasma chemistry model has been modified to incorporate non-empirical scaling of the nanosecond discharge pulse energy coupled to the plasma with number density, as well as one-dimensional conduction heat transfer. These modifications allow prediction of time-dependent temperature distribution across the plasma, without the use of the pulse energy as an adjustable parameter.

The rate of heat release, and corresponding temperature rise, as a function of the number of pulses in a burst, was predicted by the model and found to agree well with centreline pure rotational time-resolved CARS temperature measurements, in air and in ethene–air mixtures at φ = 0.1 and φ = 1.0. Comparison of centreline CARS temperatures and spatially averaged temperatures inferred from N₂ second positive emission spectra confirm that at long discharge burst duration, temperature distribution in the plasma is strongly affected by heat transfer.

Both CARS measurements and the air–fuel plasma chemistry model predictions show accelerated heating in ethene–air mixtures due to heat release during plasma chemical fuel oxidation, which is triggered by relatively fast low-temperature reactions of ethene with atomic oxygen. The initial heating rate in air–fuel plasmas is primarily controlled by the rate of radical, particularly O atom, generation and is nearly independent of the equivalence ratio. At long burst durations, the heating rate in lean ethene–air mixtures is significantly reduced at the point when nearly all of the fuel is oxidized. On the other hand, temperature in the stoichiometric ethene–air mixture continues to rise even for long burst durations due to continuous fuel oxidation/energy release process. Experimental centreline temperatures in stoichiometric ethene–air mixtures at long burst durations are observed to be higher than predicted by the model, likely due to the use of a cold wall (T_w = 300 K) boundary condition by the model, which overpredicts the rate of heat transfer from the plasma thermal to the test section walls.

Future work will include additional CARS temperature measurements at multiple locations (above and below centreline, and closer to the edges of the plasma) and additional O atom concentration measurements during burst mode discharge operation, particularly in lean ethene–air mixtures.

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